

BRAKE CONTROLLER AND METHOD FOR CONTROLLING A BRAKE SYSTEM

The present invention is directed to a braking controller and method for controlling
5 brakes, and more particularly, to a braking controller and method for controlling brakes of a
vehicle during cornering.

BACKGROUND

Brake control while a vehicle is turning or cornering presents unique challenges. In
10 particular, due to the angular velocity, lateral acceleration and speed differential between inner
and outer wheels of the vehicle, controlled braking during a turn provides additional
complexities as compared to straight-line braking. Existing braking-while-cornering systems
may analyze the speed differential between diagonally-oriented (i.e. inner and outer) wheels and
across axles. However, such systems do not analyze the status of each of the four wheels of a
15 vehicle, and do not analyze the slip status of the wheels which can be used to determine the
stability of the vehicle. Accordingly, there is a need for a braking controller and a method for
controlling a brake system which can analyze the status of each of the four wheels and which can
consider the slip status of the wheels.

SUMMARY

In one embodiment, the present invention is a braking controller and a method for
controlling a brake system which can analyze the status of each of the four wheels and which can
consider the slip status of the wheels. In particular, in one embodiment the invention is a control
system for controlling a brake system of a vehicle during a turn, the vehicle having four wheels.
25 The brake system is configured to selectively control brake pressure to each of the wheels and
includes a controller for monitoring a slip status of each of the four wheels during a turn. The
controller is configured to direct the brake system to independently increase, decrease, or hold
the brake pressure applied to each of the four wheels based at least in part upon slip status of
each respective wheel.

30 In another embodiment the invention is a control system for controlling a brake system of
a vehicle during a turn, the vehicle having a plurality of wheels. The brake system is configured
to selectively control brake pressure to each of the wheels, and includes a controller for

determining a corrective differential velocity which represents a velocity differential between at least one wheel on one side of the vehicle and at least another wheel on another side of the vehicle that is desired to maintain the desired heading of the vehicle. The controller is configured to direct the brake system to increase, decrease, or hold the brake pressure applied to each of the wheels based at least in part upon the corrective differential velocity.

Other objects and advantages of the present invention will be apparent from the following description and the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a top schematic representation of a vehicle including the system or method of the present invention;

Fig. 2 is a flow chart illustrating one algorithm for implementing the system or method of the present invention; and

Figs. 3-6 are schematic representations of a turning vehicle illustrating various oversteer and understeer conditions.

DETAILED DESCRIPTION

The present invention may be a brake system 8 which may include or be utilized in a vehicle such as the vehicle 10 schematically shown in Fig. 1. The vehicle 10 may include a set of four wheels 12, 14, 16 and 18, with each wheel 12, 14, 16, 18 having an associated brake or brake subsystem 20, 22, 24, 26. Each brake 20, 22, 24, 26 may be a hydraulically operated brake that is coupled to a hydraulic control unit or master cylinder 66 by an associated control line 44, 46, 48, 50. The master cylinder 66 may have a sensor 94 that is operatively coupled to a controller, such as an electronic control unit 68, via signal line 96. The brake system 8 may include wheel speed sensors 28, 30, 32, 34 that can monitor the rotational speed of each of the wheels 12, 14, 16, 18. The wheel speed sensors 28, 30, 32 and 34 may be operatively coupled to the controller 68 via connection lines 36, 38, 40, 42, respectively.

The brake system 8 may further include a brake pedal 64 and a brake pedal switch 82 which can determine the position of the brake pedal 64. The brake pedal switch 82 is operatively coupled to the controller 68 via signal line 84 to so that the brake pedal switch 82 can send signals indicative of the position of the brake pedal 64 to the controller 68. The brake pedal 64

may also be directly (i.e. hydraulically, mechanically, electronically or otherwise) coupled to the master cylinder 66, as indicated by the dotted line connection 65 to control the pressure in the master cylinder 66 and in the brake subsystems 20, 22, 24, 26. The brake system 8 may optionally include a brake pedal extended travel sensor 85 which can send a signal to the controller 86 via signal line 83 upon extended travel of the brake pedal 64. The brake pedal extended travel sensor 85 may be a switch that provides an output signal when the pedal 64 has been depressed an extended amount indicating "hard" braking by the driver.

The vehicle 10 includes a steering wheel 60 and a steering wheel sensor 61 to track the rotational position or angle of the steering wheel 60 and send a signal indicative of the rotational position of the steering wheel 60 to the controller 68 via signal line 62. In one example, the steering wheel position sensor 61 may be a digital sensor that provides output signals that increment a digital position signal within controller 68 with each degree or partial degree of rotation of the steering wheel 60 in one direction and decrement the digital position signal with each degree or partial degree of rotation in the opposite direction. The steering wheel sensor 61 may also be an analog sensor that provides an analog sensor position output (i.e., from a rotary resistive device of a known type).

The vehicle 10 may include a yaw rate sensor 80 which can send signals indicative of the yaw rate of the vehicle 10 to the controller 68 via signal line 81. The vehicle 10 may include the master cylinder pressure sensor 94 which can send signal indicative of the pressure of the master cylinder 66 to the controller 68 via signal line 96. The vehicle 10 may include a lateral accelerometer 98 that can send a signal to the controller 68 that is indicative of the lateral acceleration of the vehicle 10 via signal line 99. Various other sensors that provide information relating to the stability, speed or velocity of the vehicle, road and ambient conditions or driver requested headings and the like may also be utilized but are not specifically illustrated herein.

The controller 86 may include or be coupled to a vehicle stability enhancement system (VSE) 87, also referred to as an electronic stability program (ESP), which may be an electromechanical control system designed to monitor and influence wheel dynamics, and ultimately vehicle dynamics during a vehicle state of braking, accelerating or coasting. VSE 87 typically uses input from the brake sensors 28, 30, 32, 34, the steering wheel angle sensor 61, the yaw rate sensor (or vehicle rotation rate sensor) 80 and the lateral acceleration sensor (or lateral accelerometer) 98 to determining the driver's intended heading and the vehicle's actual heading.

In other words, VSE 87 may be designed to identify the intent of a driver by measuring the steering wheel angle, brake and throttle positions and vehicle speed. VSE 87 typically may control the application of the wheel brakes 20, 22, 24, 26, as necessary, to help a driver regain control in a skid caused by oversteering or understeering during a turn. However, the present invention does not rely upon the VSE 87 to provide any control of brakes, but instead may utilize the VSE 87 merely to provide processed information and data to the system/method of the present invention. The microcontroller functions for the VSE 87 may be contained in controller 68, in which case the VSE 87 need not necessarily be viewed as a separate component from the controller 68.

As part of its calculations the VSE may determine a Delta Velocity Left Right (“DVLR”) term or value. During a turn, the velocity differential between the inside wheels and the outside wheels may be monitored. DVLR represents a velocity adjustment calculated by the VSE that is required/recommended in order to ensure that the vehicle travels in the heading desired by the user. For example, in left turn in an oversteer condition, the VSE may calculate a DVLR value that requires braking of the outside (right) wheels. If the vehicle 10 is in neither an oversteer or an understeer condition (that is, the vehicle is heading where the driver desires) then the DVLR value may be zero. Various methods for determining DVLR may be utilized such as those disclosed in U.S. Pat. No. 5,720,533 and U.S. Pat. No. 5,746,486, the contents of which are hereby incorporated by reference.

DVLR may be visualized, in a simple manner, as a table or tables (typically represented in a speed such as kilometers per hour or miles per hour) that provides a value for DVLR based upon various inputs such as the speed of the vehicle, the heading desired by the driver (i.e. as determined by the steering sensor 61) and the yaw rate (as determined by the yaw rate sensor 80), and/or lateral acceleration (as determined by the accelerometer 98). The sign of DVLR may be positive or negative, depending upon the direction of turn of the vehicle and the type of velocity differential required between the left and right wheels.

The present invention performs an active brake monitoring/control of the brakes 20, 22, 24, 26 responsive to the slip status of each wheel 12, 14, 16, 18 and the instability of the vehicle 10 (or the effects proposed action will have upon instability of the vehicle 10). For a given wheel, a series of calculations are carried out in a series of closed loops to determine the slip value for that wheel. These calculations may be carried out in a processor, hardware, software,

ROM, RAM or the like in the controller 68, VSE 87 or elsewhere in the system when the vehicle is in a turn and the brakes are being applied.

For example, steps which may be used to calculate the slip value for a wheel under consideration are provided below. As a first step, a Yaw Velocity Compensation is calculated as follows:

$$\text{Yaw Velocity Compensation} = \text{track} * \text{yaw rate} \quad (\text{Eq. 1})$$

where “track” represents the width of the vehicle 10 and yaw rate represents the yaw rate of the vehicle as provided, for example, from the yaw rate sensor 80. In order to get a “true” value of the velocity contributed by the yaw of the vehicle 10 at the wheel under consideration, the right side of Equation 1 should be multiplied by $\frac{1}{2}$. However, as will be seen below this $\frac{1}{2}$ factor may be incorporated in subsequent calculations.

Next, a DVLRL value is obtained from, for example, the VSE 87. An adjusted vehicle speed is then calculated as follows:

$$\text{Adjusted Vehicle Speed} = \text{Vehicle Speed} + \text{DVLRL} - (\text{Yaw Velocity Compensation} * k1) \quad (\text{Eq. 2})$$

where Vehicle Speed represents the linear speed of the vehicle 10 at its center of gravity and $k1$ is a constant. The linear speed of the vehicle 10 at its center of gravity may be determined in a variety of manners well known to one of ordinary skill in the art, including taking an average of the wheel speed sensors 28, 30, 32, 34 or other calculation methods. The DVLRL value may be included in Equation 2 because the value represented by DVLRL may be desired to be included in subsequent slip calculations. However, if desired DVLRL may be omitted from Equation 1. As its nominal value, $k1$ may be set to $\frac{1}{2}$ to accommodate the $\frac{1}{2}$ factor discussed above in the context of Equation 1 above. However, the value for $k1$ may be adjusted as desired to increase or decrease the effect of the yaw of the vehicle upon the Adjusted Vehicle Speed. Adjusted Vehicle Speed generally represents the speed of the vehicle at the wheel that is being examined, but the Adjusted Vehicle Speed may also consider the DVLRL value.

Next, the slip of the wheel under examination is determined. The slip may be calculated as follows:

$$\text{Slip} = (\text{Adjusted Vehicle Speed} - \text{Wheel Speed}) / \text{Adjusted Vehicle Speed} \quad (\text{Eq. 3})$$

where Wheel Speed is the speed of the wheel under examination as provided by the associated wheel speed sensor 28, 30, 32, 34. Thus the slip of a wheel provides an indication of the slipping or skidding of the wheel, and is indicative of whether intervention is required. For example, a slip value of 0 (0%) indicates no skidding of the wheel; a slip value of 1 (i.e. 100%) indicates complete skidding or a “lock-up” of the wheel; a slip value of 0.1 (i.e. 10%) indicates significant braking.

Once values for slip and DVL_R are determined, the system may then enter an algorithm to determine whether brake pressure for the wheel under examination should be modified. As shown at Fig. 2, the system begins at block 100 and at block 102 the brake system enters a “hold” state. The hold state is the default state for this algorithm, and the remaining steps are utilized to determine whether the brakes depart from the hold state (i.e. whether the brakes should be applied or released). In its physical application, if the algorithm of Fig. 2 does in fact determine that the brakes should be applied or released, the application or release will occur very quickly such that the brakes may not necessarily be physically “held” or actually have sufficient time to enter a hold state at block 102. Thus the hold state at block 102 may be provided more as a conceptual default rather than a physical “holding” of the brakes, although due to a relatively quick switch time for valves the brakes may actually be held at step 102.

At block 104 it is examined whether the slip value for the wheel under examination is greater than a first slip threshold (Threshold_1). If the slip is determined to be greater than the first slip threshold, then the system proceeds to block 106 and the brake for that wheel is released. The value for the first slip threshold may be set to nearly any value as desired to provide the desired characteristics to the system/method of the present invention, and in one case may be between about 1% and about 20%, and more particularly about 10%.

The release algorithm at block 106 can be implemented in a wide variety of manners. In one case, the brake(s) to the wheel of interest are released for a period of time, and the system then waits for a brief period of time before proceeding. For example, at block 106 the brake may be released for 8 ms and the system may then rest for 32 ms. This rest period allows time for the release of the brake to effect the vehicle before the system loops again to determine whether any

further corrective action is required, and if so, what sort of corrective action is required. The system control implemented at blocks 104, 106 may be visualized as a release that is implemented when the wheel slip gets too high. After the system exits block 106 the system returns to block 100 and repeats.

5 If, at block 104 it is determined that the slip value for the wheel is not greater than the first slip threshold, the system proceeds to block 110. At block 110 it is examined whether the slip value for the wheel under examination is greater than a second slip threshold (Threshold_2). Although the second slip threshold may be set at any desired level to provide the appropriate/desired control, in most cases it is expected that the second threshold will be less
10 than the first threshold. In one case the second threshold may be between about 1% and about 20%, and more particularly about 5-7%.

 If the slip is determined to be greater than the second slip threshold at block 110, then the system proceeds to block 112 and the instability of the system is examined. One way to determine instability is to examine the magnitude and sign of the DVL_R value. Thus, as an
15 example, if the vehicle is in a left turn, the value for DVL_R may be compared to a first DVL_R threshold to determine whether DVL_R is greater than (or less than, depending upon sign conventions) the first DVL_R threshold. For example, in a left turn a positive DVL_R value may indicate that the speed of the right side of the vehicle should be decreased and/or the speed of the left side of the vehicle should be increased (if possible) in order to increase the stability of the
20 vehicle. Thus, a sufficiently large positive DVL_R value during a left turn, when coupled with a sufficiently high slip value, indicates that the brakes on the right side of the vehicle should be applied and the brakes on the left side of the vehicle should be released. This situation is illustrated in Fig. 3, using the convention that the wheels on the right side of the vehicle are solidly shaded (representing application of the brakes to those wheels) and the wheels on the left
25 side of the vehicle are shown in dotted lines (representing release of the brakes to those wheels).

 Thus in a left turn a sufficiently large positive DVL_R value is indicative of an oversteering condition and when the wheel under consideration is on the left side of the vehicle then the brakes for that wheel may be desired to be released (i.e. the system may proceed to block 114). In a right turn the DVL_R value may be a negative value, which may be indicative of
30 understeering. Thus when the value for DVL_R is a negative value having a sufficiently high

magnitude or absolute value, then the brake for the left wheel may be desired to be released (see Fig. 4).

Thus, at block 112 the following statement or equation may be used for a left wheel to determine whether instability is indicated and whether the system should proceed to the release algorithm:

$$\text{If } ((\text{Left Turn}=\text{True}) \text{ and } (\text{DVL R} > \text{DVL R Threshold1})) \text{ or } ((\text{Left Turn}=\text{False}) \text{ and } (\text{DVL R} < \text{DVL R Threshold2})) \quad (\text{Eq. 4})$$

Thus, the first portion of Equation 4 represents the situation illustrated in Fig. 3 and the second portion of Equation 4 represents the situation illustrated in Fig. 4. The values for the DVL R Thresholds may be set to adjust the desired characteristics of the method and system, and may have a wide range of values. In one embodiment, the DVL R Thresholds may have values of between about 2-50 kph, or more particularly, between about 3-7 kph. Thus, if Equation 4 is true the system may proceed to block 114 and to Release Algorithm₂. Release Algorithm₂ may be the same brake release procedure as Release Algorithm₁ or it may be a different release algorithm, depending upon the desired characteristics of the system and method. After the system exits block 114 the system returns to block 100 and repeats.

As noted above, Equation 4 may be utilized for a left wheel. If the wheel under examination is a right wheel, the following equation or statement may be utilized:

$$\text{If } ((\text{Left Turn}=\text{True}) \text{ and } (\text{DVL R} < \text{DVL R Threshold3})) \text{ or } ((\text{Left Turn}=\text{False}) \text{ and } (\text{DVL R} > \text{DVL R Threshold4})) \quad (\text{Eq. 5})$$

Thus, the first portion of Equation 5 represents the situation illustrated in Fig. 5 and the second portion of Equation 5 represents the situation illustrated in Fig. 6. Of course, Equations 4 and 5 are illustrative of merely one manner in which it can be determined whether it would be advantageous to release the wheel of interest, considering, for example, a DVL R value. Various other methods for determining whether it would be advantageous (i.e. to increase stability or ensure the vehicle attains the desired heading) to release the brake to the wheel of interest may be used without departing from the scope of the invention.

Returning to block 110, if it was determined that the slip was not greater than slip Threshold₂, then the system proceeds to block 118 wherein it is examined whether the slip value

for the wheel under examination is less than a third slip threshold (Threshold₃). If the slip is determined to be less than the third slip threshold, then the system proceeds to block 120 and the brake for that wheel is applied. The value for the third threshold may be set to nearly any limit as desired to provide the desired characteristics to the system/method of the present invention, and in one case may be between about 1% and about 20%, and more particularly about 2-3%.

The apply algorithm at block 120 can be implemented in a wide variety of manners. In one case, the brakes to the wheel of interest are applied for a period of time, and the system then waits for a brief period of time before proceeding. For example, at block 120 the brake may be applied for 5 ms and the system may then rest for 35 ms. This rest period allows time for the application of the brake to effect the vehicle before the system loops again to determine whether any further corrective action is required and if so what sort of corrective action is required. After the system exits block 120 the system returns to block 100 and repeats.

However, before the apply algorithm at block 120 is entered, the system may first implement a check. For example, the desired pressure in the master cylinder 66, as requested or desired by the driver, may be stored and noted, and the system may be monitored to ensure that the pressure in the master cylinder 66 is not increased beyond that requested by the driver. In other words, if the Apply Algorithm of block 120 would increase the pressure in the master cylinder 66 beyond that requested by the driver then block 120 may be bypassed.

Furthermore, if desired, this check step may be omitted. Because the system/method of the present invention may not include or utilize any pumps, any request from the system/method to increase the pressure beyond that in the master cylinder 66 may not have any physical effect since the system/method may lack any structure or means for increasing the pressure in the brake system beyond that in the master cylinder 66.

The system control implemented at blocks 118, 120 may be visualized as an "apply" step that is implemented when the wheel slip gets too low. In other words, blocks 118 and 120 may be visualized as a system to increase braking pressure to ensure the vehicle is decelerated as quickly as possible to match the performance requested by the driver.

If, at block 118, it is determined that the slip value for the wheel under examination is not less than the third slip threshold, the system proceeds to block 122. At block 122 it is examined whether the slip value for the wheel under examination is less than a fourth slip threshold (Threshold₄). Although the fourth slip threshold may be set at any desired level to provide the

appropriate/desired control, in most cases it is expected that the fourth slip threshold will be greater than the third slip threshold. In one case the fourth threshold may be between about 1% and about 20%, and more particularly about 5-7%.

If at block 122 the slip is determined to be less than the fourth threshold, then the system proceeds to block 124 and the instability of the system is examined. The instability of the vehicle may be examined in a manner similar to that outlined above with respect to block 112, but at block 124 it is considered whether application of a brake to the wheel of interest may increase stability.

Thus, in one case, if the vehicle is in a left turn and the wheel under consideration is the right wheel, the value for DVLR may be compared to a DVLR threshold to determine whether DVLR is greater than (or less than, depending upon sign conventions) the DVLR threshold. For example, as shown in Fig. 3, a sufficiently large DVLR value in a left turn may indicate that the speed of the right side of the vehicle should be decreased in order to increase the stability of the vehicle. Thus, a positive DVLR value may indicate that the brakes on the right side of the vehicle should be applied.

Thus in a left turn a positive DVLR value may be indicative of an oversteering condition. When the value for DVLR is sufficiently large, and the wheel under consideration is on the right side of the vehicle, then the brake(s) for the right wheel may be desired to be applied (i.e. the system may proceed to block 126).

In a right turn a negative DVLR value may be indicative of an understeering condition. Thus when the value for DVLR is a negative value having a sufficiently high magnitude or absolute value, then the brake(s) for the right wheel may be desired to be applied, as shown in Fig. 4.

Thus, at block 124 the following statement or equation may be used for a right wheel to determine whether instability is indicated and whether the system should proceed to an apply algorithm:

$$\text{If } ((\text{Left Turn}=\text{True}) \text{ and } (\text{DVLR} > \text{DVLR Threshold5})) \text{ or } ((\text{Left Turn}=\text{False}) \text{ and } (\text{DVLR} < \text{DVLR Threshold6})) \quad (\text{Eq. 6})$$

Thus, the first portion of Equation 6 represents the situation illustrated in Fig. 3 and the second portion of Equation 6 represents the situation illustrated in Fig. 4. The values for the

DVLR Thresholds of Equation 6 may be set to adjust the desired characteristics of the method and system, and may have a wide range of values. In one embodiment, the DVLR Thresholds 5 and 6 may have values of between about 2-50 kph, or more particularly, between about 3-7 kph.

Equation 6 has the same general form as Equation 4, although the values for the DVLR

5 thresholds may differ, if desired. Thus, if Equation 6 is true the system may proceed to block 126 and to Apply Algorithm₂.

Apply Algorithm₂ may be the same brake apply procedure as Apply Algorithm₁ or it may be a different apply algorithm, depending upon the desired characteristics of the system and method. Furthermore, the same checks outlined above to ensure that the applied pressure does
10 not exceed the pressure in the master cylinder may be utilized before the system proceeds to the Apply Algorithm of block 126.

As noted above, Equation 6 may be utilized for a right wheel. If the wheel under examination is a left wheel, the following equation or statement may be utilized:

15 If ((Left Turn=True) and (DVLR<DVLR Threshold7)) or ((Left Turn=False) and (DVLR>DVLR Threshold8)) (Eq. 7)

Thus, the first portion of Equation 7 represents the situation illustrated in Fig. 5 and the second portion of Equation 7 represents the situation illustrated in Fig. 6. Equation 7 has the
20 same form as Equation 5, although the values for the DVLR thresholds may differ, if desired. Of course, Equations 6 and 7 are illustrative of merely one manner in which it can be determined whether it would be advantageous to apply the brake(s) to the wheel of interest, considering, for example, the DVLR value. Various other methods for determining whether it would be advantageous (i.e. by increasing stability or ensuring the vehicle attains the desired heading) to
25 apply the brake to the wheel of interest may be used without departing from the scope of the invention. After the system exits either block 122 or block 126 the system returns to block 100 and repeats.

The system may be implemented upon all four wheel 12, 14, 16, 18 of a vehicle 10 simultaneously or upon each of the wheels in sequential order. Thus, for example, the flow chart
30 of Fig. 2 may be utilized in series for all four wheels, or may be utilized simultaneously (i.e. in parallel) for each wheel. Further, the system may be implemented in a vehicle having more or

less than four wheels. The system and method increases stability of the vehicle and performance of the vehicle, and does not require pumps or boosters in the brake system. Individual control can be exerted over each of the four wheels to provide more accurate control.

5 Further, each of the thresholds discussed herein (for example, slip threshold₁, slip threshold₂, slip threshold₃, slip threshold₄, DVL_R thresholds 1-8, etc.) may not necessarily be fixed values, but may be dynamic or variable thresholds which can be set on the fly to change the operating characteristics of the system or method. The various thresholds may be set by taking into account a wide variety of factors, such as wheel slip, applied brake pressure, DVL_R, etc. Furthermore, each threshold may be set or calculated independently for each wheel under
10 examination. Finally, the closed-loop control system and method of the present invention provides continuous monitoring and feedback during a turn.

Having described the invention in detail and by reference to the preferred embodiments, it will be apparent that modifications and variations thereof are possible without departing from the scope of the invention.

15 What is claimed is: